

# TECHNICAL DATA SHEET

## PRESSURE ON CARBON BRUSHES

### 01 - BASIC PRINCIPLES

The **pressure exerted** should be **sufficient to ensure continuous contact** of the brush on the slip ring or commutator under all working conditions of the machine.

**Contact loss** between the brush and the slip ring or commutator is the cause of sparking under the brush. This sparking causes damage to the commutator or slip ring and accelerated brush wear.

This basic principle leads to the following logical consequence.

The optimum brush pressure is a combination of both electrical and mechanical considerations. Since the requirements of these considerations are often contradictory, the suitable pressure is, therefore, a compromise (Fig.1).

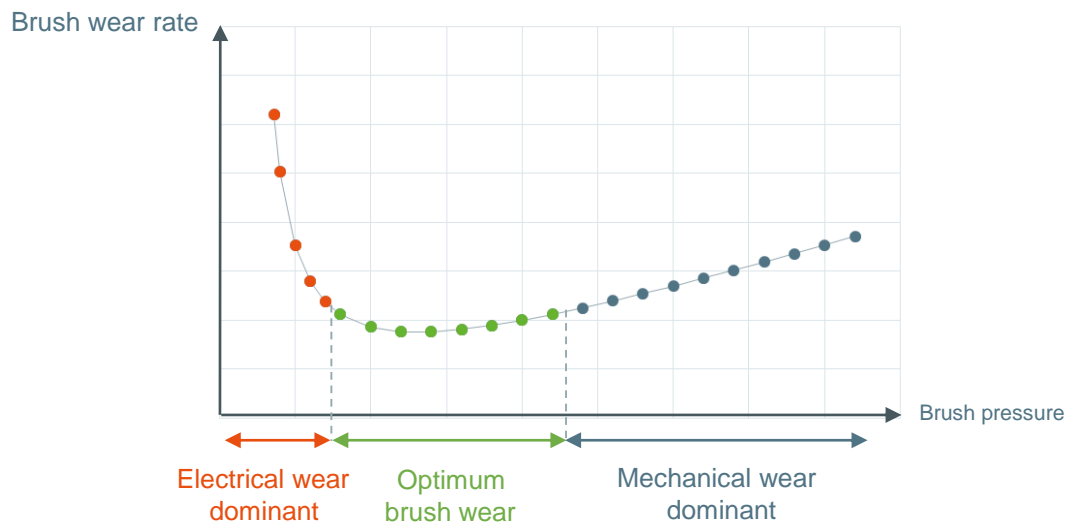


Figure 1 – Brush wear as a function of brush pressure

For machines which are:

- subject to shocks and vibrations (such as traction motors, motors for propellers, exciters, etc.),
- or machines with poor stability (unbalance, out of round),

**the brush spring pressure should be increased** to prevent the additional risks of interruption of commutator or slip ring brush contact.

**02 - MECHANICAL**

The **mechanical losses**, and therefore the temperature and wear of brushes, **increase** with the pressure.

The **maximum tolerable pressure** for a brush **depends on the hardness of the material**. Recommended brush pressure depending on grade family is presented in table 2.

All soft or fragile brushes are eliminated from applications requiring high pressure (i.e. higher than 225 kPa). In the group of unsuitable grades one would find particularly the soft natural graphite grades (LFC).

The above considerations proves the advantage of brush holders with stable pressure or at least brush pressure systems which guarantee a low variation of brush pressure during the life of the brush.

**03 - ELECTRICAL**

The **contact voltage drop** under the brush **decreases when the pressure is increased**.

Consequently for a DC machine the commutating properties of the brush decrease at higher pressures.

This decrease in contact drop, with pressure increase, should not be considered as insignificant. For an electrographitic brush (at 10 A/cm<sup>2</sup> and 30 m/s) it can reach 30 % when the pressure goes from 15 to 55 kPa.

Based on this, please, note that the coefficient  $k_p$  allows to calculate the pressure  $P$  (in kPa), the evaluation of the voltage contact drop  $U_p$  (in mV) for a reference pressure  $P_0$  (for instance 15 kPa), by the formula:

$$\Delta U_p = k_p \times \Delta U_{p0}$$

where:

$\Delta U_{p0}$  is the voltage contact drop at the reference pressure  $P_0$  in mV.

$k_p$  is not a constant coefficient and is always lower than 1: its value decreases faster for lower pressures than for higher pressures. The table below gives some values of this coefficient resulting from laboratory tests carried out on an electrographitic brush at 10 A/cm<sup>2</sup>.

P (kPa)	15	25	35	45	55	65	75
$k_p$	1	0.90	0.82	0.76	0.71	0.67	0.64

Table 1 - Values of coefficient  $k_p$  according to brush pressure for a standard EG grade at 10A/cm<sup>2</sup>

The effect is extremely important especially for commutators with large chamfers on the bar edges (increased spacing compared with the useful width of the bars), as for slip rings with helical grooves.

**04 - RECOMMENDED SPRING PRESSURE**

Recommended spring pressure P for each grade family	Slip ring	Commutator	
		Stationary machines	Traction machines
Carbographic (amorphous or hard)		18 – 20	
Electrographitic	18 – 20	18 – 20	36 - 45
Resin impregnated electrographitic	*	18 – 20	36 - 55
Soft graphitic	11 – 20*	13 – 18	
Metal-graphite	rated speed	18 – 20	*
	speed < 1m/s	25 – 27	

Note about units: 1 kPa = 10 cN/cm², which is approximately 10 g/cm² (1kgF=9.81N), 1.500 PSI

Table 2 - Recommended spring-pressures (in kPa) under normal operating conditions

\* Please consult us  
\*\* For forklift motors

**05 - SPECIFIC SPRING PRESSURE**

Specific brush pressure *p* is the force applied on brush per area. It can be easily calculated from the force and brush section by the formula:

$$p = \frac{F_r}{t \times a}$$

where:

*F<sub>r</sub>* is the measured force, in grams (respectively cN).

*t* and *a* are the tangential and axial dimensions of the brush, in cm.

Specific brush pressure is given in g/cm² (respectively cN/cm²).

**REMARKS**

- The surface considered as the basis of calculation for the pressure indicated above does not take into account the empty space under the brush (that is to say: space between the bars of the commutator, helical grooves of slip rings, oblique saw cuts in the contact faces of the brushes for rings without groove) but only the cross section of the brush.
- It should be noted that in the case of grooved slip rings, the contact surface should be reduced by the width of the groove under the brush. The formula of specific brush pressure *p* becomes:

$$p = \frac{F_r}{t \times (a - k \times b)}$$

where:

*b* is the groove width and *k* is the number of grooves under the brush (see TDS-03)

- For bevelled brushes the pressures are calculated from the cross section and the real surface of the contact face is generally not used for the base of calculation.

Nevertheless it shall be taken into account when calculating mechanical losses (see TDS-05).

For a brush with a contact bevel angle *α* (see TDS-04), *p* is given by the formula:

$$p = \frac{F_r}{t \times a \times \cos \alpha}$$

## 06 - BRUSH PRESSURE MEASUREMENT

**Periodic measurement** of brush pressure, by a spring balance or a load-cell (dynamometer), is strongly recommended.

The IEC Technical Report IEC 61015 specifies the methods for measurement of the force applied on the brush.

Pressure shall be **similar for all brushes** to ensure a good current distribution. Uneven brush pressure between brushes may cause specially an uneven distribution of current on the same arm (on commutator) or same ring, and overloading on some individual brush. The result may be uneven brush wear, brush damage, over-heated flexibles and tamping failure with associated grooving.

**A relative difference of 15% maximum is acceptable.**

*Associated literature:*

*IEC 61015/TR: "Brush-holders for electrical machines – Guide to the measurement of static thrust applied to brushes"*

*TDS-03: Chamfering of commutator bar edges - Machining of ring helical grooves*

*TDS-04: Dimensions of carbon brushes and brush-holders*

*TDS-05: Losses in carbon brushes*

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CL-DynamoMeter used with V-block magnetic foot

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